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ORIGINAL ARTICLE Modelling of occupational exposure to inhalable nickel compounds

Benjamin Kendzia^{1,5}, Beate Pesch^{1,5}, Dorothea Koppisch², Rainer Van Gelder², Katrin Pitzke², Wolfgang Zschiesche¹, Thomas Behrens¹, Tobias Weiss¹, Jack Siemiatycki³, Jerome Lavoué³, Karl-Heinz Jöckel⁴, Roger Stamm² and Thomas Brüning¹

The aim of this study was to estimate average occupational exposure to inhalable nickel (Ni) using the German exposure database MEGA. This database contains 8052 personal measurements of Ni collected between 1990 and 2009 in adjunct with information on the measurement and workplace conditions. The median of all Ni concentrations was 9 μ g/m³ and the 95th percentile was 460 μ g/m³. We predicted geometric means (GMs) for welders and other occupations centered to 1999. Exposure to Ni in welders is strongly influenced by the welding process applied and the Ni content of the used welding materials. Welding with consumable electrodes of high Ni content (>30%) was associated with 10-fold higher concentrations compared with those with a low content (<5%). The highest exposure levels (GMs $\ge 20 \,\mu$ g/m³) were observed in gas metal and shielded metal arc welders using welding materials with high Ni content, in metal sprayers, grinders and forging-press operators, and in the manufacture of batteries and accumulators. The exposure profiles are useful for exposure assessment in epidemiologic studies as well as in industrial hygiene. Therefore, we recommend to collect additional exposure-specific information in addition to the job title in community-based studies when estimating the health risks of Ni exposure.

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INTRODUCTION

Exposure to nickel (Ni) is a widely distributed exposure circumstance in the production and processing of steel or alloys, for example, in foundry workers and welders. The International Agency for Research on Cancer classified exposure to metallic Ni and nickel-containing alloys as possibly carcinogenic (Group 2B).¹ Exposure to Ni and its compounds in Ni refining was classified as carcinogenic to humans (Group 1).² Compared with the production of nearly 800 million tons of steel, only 1.4 million tonnes of primary Ni are mined, smelted or refined currently in about 25 countries,³ but not in Germany. Furthermore, Ni is used in the production of batteries and accumulators, and in some other applications.

Nickel occurs in the metallic form as oxides and mixed oxides (spinels) in welding fumes and in a variety of compounds in the ore or in industrial applications. Bioavailability is influenced by the solubility of the Ni species, where oxides and sulfides are poorly soluble compared with certain nickel salts.⁴ The European Scientific Committee on Occupational Exposure Limits (SCOEL) considered both, soluble and insoluble particulate Ni compounds as carcinogenic to humans, but not metallic Ni.⁵

Several governmental and scientific agencies have recommended occupational exposure limits (OELs) for Ni and its compounds. The current 8 h time-weighted average permissible exposure limit (PEL) of the US Occupational Safety and Health Administration for metallic Ni and insoluble Ni compounds is 1000 μ g/m³ in total dust.⁶ SCOEL proposed 10 μ g/m³ for all forms of Ni in inhalable particles, excluding metallic Ni, to protect workers from Ni carcinogenicity.⁵ However, Ni is a frequent cause of allergic contact dermatitis, induced by even smaller concentrations. In Germany, 6 μ g/m³ is the recent OEL for respirable Ni in its metallic form to protect workers from irritative effects.⁷

So far, dose–response relations of exposure to Ni with lung cancer were predominantly investigated in the Ni refining industry.^{8–11} By contrast, welders comprise a much larger workforce and are exposed to Ni within a complex welding fume matrix consisting of spinels and metal oxides. It is yet challenging to disentangle the lung cancer risk associated with exposure to welding fume into its major components Ni, hexavalent chromium (Cr(VI)) and particulate matter. A welding-process exposure matrix was developed to estimate exposure to Ni and other agents in a cohort study of welders, but few measurements were available to support the quantitative estimates.^{12,13}

The exploration of large exposure databases may improve exposure assessment.¹⁴ Here we took advantage of the comprehensive exposure database MEGA (Messdaten zur Exposition gegenüber Gefahrstoffen am Arbeitsplatz)¹⁵ to estimate the mean concentration of Ni related to job tasks and industrial settings, allowing for a refinement or validation of existing JEMs, especially for major welding processes.

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METHODS

Measurements of inhalable nickel

Airborne concentrations of inhalable Ni were compiled together with information on the duration of measurement, the analytical method, and the workplace in the MEGA exposure database at the Institute for Occupational Safety and Health of DGUV (IFA).^{15,16} This analysis was based on 8052 personal Ni measurements taken between 1990 and 2009. Airborne dust was collected on glass fibre, quartz-glass fibre or cellulose nitrate filters with a GSP sampler operating at a flow rate of 3.5 l/min according to the European standard EN 481, to capture inhalable particles.¹⁷ This particle fraction is defined as the mass fraction of particles, which can be inhaled by nose or mouth. Particles > 100 μ m are not included in this convention.

The filters were shipped to the central laboratory at IFA for quantitative Ni determination with different analytic methods. Ni was determined after digestion with standard digestion agent according to a protocol of Deutsche Forschungsgemeinschaft.¹⁸ The filters were digested with a mixture of nitric and hydrochloric acid, and following dilution before quantitive analysis with different analytical techniques.

Flame atomic absorption spectrometry (FT-AAS) and graphite furnace AAS (ETA-AAS) were the standard methods in the early 1990ies. ETA-AAS achieves lower limits of quantification (LOQs). This more sensitive method was additionally applied to determine Ni, especially in low-exposure circumstances to comply with EN 482. Total reflection X-ray fluorescence and the more sensitive inductively coupled plasma mass spectrometry were increasingly applied as multi-element methods since 1996. Ni was also determined with inductively coupled plasma optical emission spectrometry since 2006.

Measurements below the LOQ were documented by their individual LOQs, which mainly depend on the analytical method used, pump flow rate and duration of sampling.

Assessment of settings with occupational exposure to nickel

All workplaces were documented according to the national classification of occupations,¹⁹ together with a description of job tasks and occupational settings. We classified welders by the predominantly applied welding process and the Ni content of the welding consumable or of the base material in consumable-free techniques (<5%, 5–30% and >30%). Another 12 occupational tasks were classified as "metal workers" (cutters,

metal sprayers, electroplaters, foundry workers, grinders, polishers, solderers or brazers, surface coaters, forging-press operators, scrap-metal workers and sinters). Other settings comprised the manufacture of accumulators and batteries, and rare exposure circumstances in the chemical industry and glass production. All assignments of measurements to the pre-defined job tasks were classified independently with 96% agreement (BK, BP and DK). A random subset of 100 ambigous assignments was subjected to an additional rating (WZ). Measurements that could not be assigned to these settings were classified as "other occupations."

Statistical analysis

All calculations were performed with the statistical software SAS, version 9.4 (SAS Institute, Cary, NC, USA). We present the distribution of Ni concentrations with the fraction of measurements below LOQ, the 75th,



Figure 1. Density function of the concentrations of inhalable nickel (MEGA (Messdaten zur Exposition gegenüber Gefahrstoffen am Arbeitsplatz) database, 1990–2009).

Characteristics	Ν	N < LOQ (%)	Median (µg/m³)	P75 (μg/m³)	P90 (μg/m³)	P95 (μg/m³)
Total	8052	27	9	50	210	460
Filter type						
Quartz-glass fibre	1017	27	5	27	130	360
Cellulose nitrate	5747	25	10	53	220	480
Glass fibre	1288	34	10	60	220	420
Analytical method						
AÁS	6023	23	10	60	230	500
ICP-OES	541	35	7	31	155	410
ICP-MS	732	30	4	20	99	270
X-ray fluorescence	756	45	7	39	160	350
Time of measurement (years)						
1990-<1994	1639	28	10	50	200	420
1994- < 1999	2321	31	10	50	210	500
1999- < 2004	1889	21	9	50	240	460
2004–2009	2203	26	7	40	180	420
Sampling time (hours)						
<2	1067	30	20	99	500	1200
2-<3	5926	26	9	50	190	400
3-<4	646	26	6	34	120	300
\geq 4	413	26	4	23	120	270

Abbreviation: AAS, atomic absorption spectroscopy; ICP-OES, inductively coupled plasma optical emission spectrometry; ICP-MS, inductively coupled plasma mass spectrometry; LOQ, limit of quantification; MEGA, Messdaten zur Exposition gegenüber Gefahrstoffen am Arbeitsplatz. P75, 75th percentile; P90, 90th percentile, P95, 95th percentile.

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90th and 95th percentile. We refrained from the presentation of the 25th percentile, because 27% of all measurements were <LOQ. Multiple imputation was performed for measurements below LOQ according to the method used for measurements of Cr(VI).^{20,21} Mixed-effects models were applied to the natural log-transformed Ni concentrations with imputed non-detects to assess the geometric means (GMs) of exposure to Ni in the various occupational settings with gas metal arc welding with solid wire (GMAW) as reference group. We adjusted by the Ni content of the welding material, duration of sampling (continuous and log-transformed) and calender year (median-centered at 1999). We refrained from adjustment of the analytical method and type of filter, which are dependent on the anticipated exposure level and calender year. We present GMs adjusted and not adjusted for the duration of sampling. The adjusted R^2 was estimated for goodness-of-fit of the regression models.²² We estimated the variability of Ni exposure between and within occupational settings using a simple one-way random-effects analysis of variance according to Loomis and Kromhout?

RESULTS

Characteristics of the 8052 personal measurements of inhalable nickel collected between 1990 and 2009 are shown in Table 1. Sampling on cellulose nitrate filter was the predominant type of particle collection (n = 5747). The major analytical method, especially in the earlier years, was AAS. Median duration of sampling was 2 h. The distribution of all concentrations (Figure 1) was skewed with a median concentration of 9 µg/m³ and a 95th percentile of 460 µg/m³.

Table 2 presents the distribution of the measurements in welders (n = 3055) and other occupations. GMAW resulted in a median concentration of 22 µg/m³ compared with 5 µg/m³ in tungsten inert gas welding (TIG). A high Ni content of > 30% of the welding material (mainly of the consumable) yielded a median Ni concentration of 74 µg/m³ for GMAW and 78 µg/m³ for

Table 2. Distribution of personal measurements of inhalable nickel in occupations with anticipated exposure (MEGA database, 1990–2009)							
Occupation	Ni content of welding material (%)	Ν	N < LOQ (%)	Median (µg/m³)	P75 (μg/m³)	P90 (μg/m³)	P95 (μg/m³)
Welder							
GMAW	Total	1159	17	22	97	250	420
	Unknown	542	21	11	78	210	380
	< 5	156	34	5	20	55	110
	5–30	405	5	50	130	320	436
	> 30	56	4	74	405	980	1600
FCAW	Total	93	25	7	29	55	155
	Unknown	66	29	5	10	30	50
	< 5	11	36	3	11	29	110
	5–30	16	0	40	139	312	460
	> 30	0	_	—	—	_	_
TIG	Total	799	28	5	14	38	82
	Unknown	330	29	6	20	46	99
	< 5	18	50	4	6	19	40
	5–30	430	27	5	12	31	60
	> 30	21	14	8	13	37	50
SMAW	Total	479	17	15	51	180	330
	Unknown	283	22	10	40	170	330
	< 5	34	21	5	45	210	1020
	5–30	140	14	20	61	143	245
	> 30	22	5	78	270	520	630
Autogenous welding		20	15	6	10	65	404
Laser welding		35	37	4	10	35	40
Submerged arc welding		26	42	5	8	24	38
Plasma welding		64	18	14	63	130	280
Resistance welding		12	50	<100	5	6	8
Others or not specified		368	26	18	60	190	320
Metal worker							
Cutter		259	18	19	120	630	1100
Metal sprayer		234	12	30	90	380	910
Electroplater		875	37	3	9	29	72
Foundry worker		350	34	6	25	170	450
Grinder		1291	22	21	120	470	1100
Chip-remove processor		133	42	5	30	170	360
Polisher/ molder		285	11	20	68	210	430
Solderer		80	63	<LOQ	9	43	160
Surface coater		112	52	< LOO	12	95	160
Forging-press operator		68	18	39	150	300	360
Scrap-metal worker		197	65	< LOO	10	50	120
Sinter		146	19	33	230	800	1100
Other exposure circumstances							
Chemical workers		183	45	7	35	230	1400
Manufacture of accumulators	i	50	4	20	60	175	350
Manufacture of batteries		219	8	30	130	370	570
Manufacture of glass		178	29	10	39	190	450
Other occupations		337	45	5	20	110	350
Other occupations		337	45	5	20	110	350

Abbreviation: FCAW, flux-cored arc welding; GMAW, gas metal arc welding; LOQ, limit of quantification; MEGA, Messdaten zur Exposition gegenüber Gefahrstoffen am Arbeitsplatz; SMAW, shielded metal arc welding; P75, 75th percentile; P90, 90th percentile; P95, 95th percentile; TIG, tungsten inert gas welding.

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 Table 3.
 Influence of occupation, year of measurement, Ni content of the welding material and sampling duration on the concentration of inhalable

 nickel (MEGA database, 1990–2009)

$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$			Model wit	th adjustment for s (R ² = 0.17)	ampling time	Model w	for sampling)	
Intercept 8052 44 36-54 27 23-33 Welder		Ν	Exp(β)	95% CI	Р	$Exp(\beta)$	95% CI	Р
Welder 1159 1.00 1.00 FCAW 93 0.51 0.31-0.83 0.0066 0.46 0.28-0.75 0.0020 TIG 799 0.21 0.17-0.26 < 0.0001	Intercept	8052	44	36–54		27	23–33	
GMAW 1159 1.00 1.00 FCAW 93 0.51 0.31-0.83 0.0066 0.46 0.28-0.75 0.0020 TIG 799 0.21 0.17-0.26 < 0.0001	Welder							
FCAW 93 0.51 0.31 0.31 0.31 0.066 0.46 0.28-0.75 0.0020 SMAW 479 0.76 0.60-097 0.0200 0.83 0.66-1.06 0.1330 Autogenous welding 20 0.46 0.17-1.23 0.1232 0.48 0.18-1.28 0.1428 Laser welding 25 0.17 0.06-0.44 0.0003 0.17 0.07-0.46 0.0001 Plasma welding 12 0.07 0.02-0.30 0.0003 0.07 0.01-0.30 0.0003 Others or not specified 368 1.06 0.84-1.34 0.6319 1.12 0.89-1.42 0.3348 Ni content of welding material (%) - - - - - - - - - 0.001 0.20 0.15-0.29 <0.0001	GMAW	1159	1.00			1.00		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	FCAW	93	0.51	0.31-0.83	0.0066	0.46	0.28-0.75	0.0020
SMAW 479 0.76 0.60-0.97 0.0260 0.83 0.66-1.06 0.1330 Autogenous welding 20 0.46 0.17-1.23 0.1232 0.48 0.18-1.28 0.1428 Laser welding 35 0.15 0.07-0.33 <0.0001	TIG	799	0.21	0.17-0.26	< 0.0001	0.21	0.17-0.26	< 0.0001
Autogenous welding 20 0.46 0.17-1.23 0.1232 0.48 0.18-1.28 0.1428 Laser welding 35 0.15 0.07-0.33 <0.0001	SMAW	479	0.76	0.60-0.97	0.0260	0.83	0.66-1.06	0.1330
	Autogenous welding	20	0.46	0.17-1.23	0.1232	0.48	0.18-1.28	0.1428
Submerged arc welding 26 0.17 0.06–0.44 0.0003 0.17 0.07–0.46 0.0004 Plasma welding 12 0.07 0.02–0.30 0.0003 0.07 0.01–0.30 0.0003 Others or not specified 368 1.06 0.84–1.34 0.6319 1.12 0.89–1.42 0.3348 Ni content of welding material (%) 0.6319 1.12 0.89–1.42 0.3348 Ni content of welding material (%) 0.6319 1.00 1.00 0.0011 0.20 0.15–0.29 <0.0001	Laser welding	35	0.15	0.07-0.33	< 0.0001	0.16	0.07-0.35	< 0.0001
Plasma welding 64 0.67 0.38-1.17 0.1629 0.74 0.42-1.31 0.3033 Resistance welding 12 0.07 0.02-0.30 0.0003 0.07 0.01-0.30 0.0003 Others or not specified 368 1.06 0.84-1.34 0.6319 1.12 0.89-1.42 0.3348 Ni content of welding material (%) 5 238 0.21 0.15-0.30 < 0.0001	Submerged arc welding	26	0.17	0.06-0.44	0.0003	0.17	0.07-0.46	0.0004
Resistance welding 12 0.07 0.02–0.30 0.0003 0.07 0.01–0.30 0.0003 Others or not specified 368 1.06 0.84–1.34 0.6319 1.12 0.89–1.42 0.3348 Ni content of welding material (%) 0.6319 1.12 0.89–1.42 0.3348 Ni content of welding material (%) 0.0001 0.20 0.15–0.29 <0.0001	Plasma welding	64	0.67	0.38-1.17	0.1629	0.74	0.42-1.31	0.3033
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Resistance welding	12	0.07	0.02-0.30	0.0003	0.07	0.01-0.30	0.0003
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Others or not specified	368	1.06	0.84–1.34	0.6319	1.12	0.89–1.42	0.3348
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Ni content of welding material (%)							
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	< 5	238	0.21	0.15-0.30	< 0.0001	0.20	0.15-0.29	< 0.0001
> 30 118 1.98 1.30-3.01 0.0015 2.30 1.51-3.51 0.0001 Unknown or no welding process 6601 0.51 0.43-0.60 < 0.0001	5–30	1095	1.00			1.00		
Unknown or no welding process 6601 0.51 0.43-0.60 < 0.0001 0.51 0.43-0.61 < 0.0001 Metal worker Cutter 259 1.03 0.74-1.44 0.8603 1.18 0.85-1.64 0.3259 Metal sprayer 234 2.48 1.69-3.63 < 0.0001 2.78 1.89-4.07 < 0.0001 Electroplater 875 0.19 0.15-0.24 < 0.0001 0.18 0.15-0.23 < 0.0001 Grinder 1291 1.82 1.48-2.23 < 0.0001 0.49 0.41-0.67 < 0.0001 Chip-remove processor 133 0.28 0.18-0.42 < 0.0001 0.28 0.19-0.43 < 0.0201 Polisher/ molder 285 0.81 0.50-1.32 0.4047 0.77 0.47-1.25 0.2826 Solderer 80 0.05 0.03-0.11 < 0.0001 0.06 0.03-0.11 < 0.0001 Surface coater 112 0.18 0.11-0.29 < 0.0001 0.08 0.05-0.11 < 0.0001 S	> 30	118	1.98	1.30-3.01	0.0015	2.30	1.51-3.51	0.0001
Metal workerCutter2591.030.74–1.440.86031.180.85–1.640.3259Metal sprayer2342.481.69–3.63<0.0001	Unknown or no welding process	6601	0.51	0.43-0.60	< 0.0001	0.51	0.43–0.61	< 0.0001
$\begin{array}{c} \mbox{Cutter} & 259 & 1.03 & 0.74-1.44 & 0.8603 & 1.18 & 0.85-1.64 & 0.3259 \\ \mbox{Metal sprayer} & 234 & 2.48 & 1.69-3.63 & < 0.0001 & 2.78 & 1.89-4.07 & < 0.0001 \\ \mbox{Electroplater} & 875 & 0.19 & 0.15-0.24 & < 0.0001 & 0.18 & 0.15-0.23 & < 0.0001 \\ \mbox{Foundry worker} & 350 & 0.53 & 0.41-0.67 & < 0.0001 & 0.49 & 0.41-0.67 & < 0.0001 \\ \mbox{Grinder} & 1291 & 1.82 & 1.48-2.23 & < 0.0001 & 1.75 & 1.42-2.15 & < 0.0001 \\ \mbox{Chip-remove processor} & 133 & 0.28 & 0.18-0.42 & < 0.0001 & 0.28 & 0.19-0.43 & < 0.0001 \\ \mbox{Chip-remove processor} & 133 & 0.28 & 0.05 & 0.03-0.11 & < 0.0001 & 0.06 & 0.03-0.11 & < 0.0001 \\ \mbox{Surface coater} & 80 & 0.05 & 0.03-0.11 & < 0.0001 & 0.06 & 0.03-0.11 & < 0.0001 \\ \mbox{Surface coater} & 112 & 0.18 & 0.11-0.29 & < 0.0001 & 0.19 & 0.12-0.31 & < 0.0001 \\ \mbox{Surface coater} & 197 & 0.07 & 0.05-0.10 & < 0.0001 & 0.08 & 0.05-0.11 & < 0.0001 \\ \mbox{Sinter} & 146 & 1.51 & 1.03-2.20 & 0.0336 & 1.48 & 1.01-2.17 & 0.0436 \\ \hline \mbox{Other exposure circumstances} \\ \mbox{Chemical workers} & 183 & 0.51 & 0.35-0.73 & 0.0003 & 0.56 & 0.38-0.81 & 0.0020 \\ \mbox{Manufacture of accumulators} & 50 & 1.58 & 0.88-2.85 & 0.1273 & 1.69 & 0.93-3.06 & 0.0823 \\ \mbox{Manufacture of glass} & 178 & 1.13 & 0.88-1.45 & 0.3528 & 1.17 & 0.91-1.51 & 0.2259 \\ \mbox{Other occupations} & 337 & 0.51 & 0.42-0.60 & < 0.0001 & 0.50 & 0.40-0.62 & < 0.0001 \\ \end{tabular}$	Metal worker							
Metal sprayer2342.481.69-3.63< 0.00012.781.89-4.07< 0.0001Electroplater8750.190.15-0.24< 0.0001	Cutter	259	1.03	0.74-1.44	0.8603	1.18	0.85-1.64	0.3259
Electroplater 875 0.19 $0.15-0.24$ < 0.0001 0.18 $0.15-0.23$ < 0.0001 Foundry worker 350 0.53 $0.41-0.67$ < 0.0001 0.49 $0.41-0.67$ < 0.0001 Grinder 1291 1.82 $1.48-2.23$ < 0.0001 1.75 $1.42-2.15$ < 0.0001 Chip-remove processor 133 0.28 $0.18-0.42$ < 0.0001 0.28 $0.19-0.43$ < 0.0001 Polisher/ molder 285 0.81 $0.50-1.32$ 0.4047 0.77 $0.47-1.25$ 0.2826 Solderer 80 0.05 $0.03-0.11$ < 0.0001 0.06 $0.03-0.11$ < 0.0001 Surface coater 112 0.18 $0.11-0.29$ < 0.0001 0.19 $0.12-0.31$ < 0.0001 Forging-press operator 68 1.86 $1.09-3.18$ 0.0220 1.86 $1.08-3.18$ 0.0242 Scrap-metal worker 197 0.07 $0.05-0.10$ < 0.0001 0.08 $0.05-0.11$ < 0.0001 Sinter 146 1.51 $1.03-2.20$ 0.0336 1.48 $1.01-2.17$ 0.0436 Other exposure circumstancesChemical workers 50 1.58 $0.88-2.85$ 0.1273 1.69 $0.93-3.06$ 0.0823 Manufacture of batteries 219 2.01 $1.47-2.76$ < 0.0001 2.05 $1.49-2.82$ < 0.0001 Manufacture of glass 178 1.13 $0.88-1.45$ 0.3528 1.17 $0.91-1.51$	Metal sprayer	234	2.48	1.69-3.63	< 0.0001	2.78	1.89-4.07	< 0.0001
Foundry worker 350 0.53 $0.41-0.67$ < 0.0001 0.49 $0.41-0.67$ < 0.0001 Grinder1291 1.82 $1.48-2.23$ < 0.0001 1.75 $1.42-2.15$ < 0.0001 Chip-remove processor133 0.28 $0.18-0.42$ < 0.0001 0.28 $0.19-0.43$ < 0.0001 Polisher/ molder285 0.81 $0.50-1.32$ 0.4047 0.77 $0.47-1.25$ 0.2826 Solderer80 0.05 $0.03-0.11$ < 0.0001 0.06 $0.03-0.11$ < 0.0001 Surface coater112 0.18 $0.11-0.29$ < 0.0001 0.19 $0.12-0.31$ < 0.0001 Forging-press operator68 1.86 $1.09-3.18$ 0.0220 1.86 $1.08-3.18$ 0.0242 Scrap-metal worker197 0.07 $0.05-0.10$ < 0.0001 0.08 $0.05-0.11$ < 0.0001 Sinter146 1.51 $1.03-2.20$ 0.0336 1.48 $1.01-2.17$ 0.0436 Other exposure circumstancesChemical workers183 0.51 $0.35-0.73$ 0.0003 0.56 $0.38-0.81$ 0.0020 Manufacture of batteries219 2.01 $1.47-2.76$ < 0.0001 2.05 $1.49-2.82$ < 0.0001 Manufacture of glass178 1.13 $0.88-1.45$ 0.3528 1.17 $0.91-1.51$ 0.2259 Other occupations337 0.51 $0.42-0.60$ < 0.0001 0.50 $0.40-0.62$ < 0.0001 <	Electroplater	875	0.19	0.15-0.24	< 0.0001	0.18	0.15-0.23	< 0.0001
Grinder12911.821.48–2.23< 0.00011.751.42–2.15< 0.0001Chip-remove processor1330.280.18–0.42< 0.0001	Foundry worker	350	0.53	0.41-0.67	< 0.0001	0.49	0.41-0.67	< 0.0001
$\begin{array}{c ccccc} \mbox{Chip-remove processor} & 133 & 0.28 & 0.18-0.42 & < 0.0001 & 0.28 & 0.19-0.43 & < 0.0001 \\ \mbox{Polisher/molder} & 285 & 0.81 & 0.50-1.32 & 0.4047 & 0.77 & 0.47-1.25 & 0.2826 \\ \mbox{Solderer} & 80 & 0.05 & 0.03-0.11 & < 0.0001 & 0.06 & 0.03-0.11 & < 0.0001 \\ \mbox{Surface coater} & 112 & 0.18 & 0.11-0.29 & < 0.0001 & 0.19 & 0.12-0.31 & < 0.0001 \\ \mbox{Forging-press operator} & 68 & 1.86 & 1.09-3.18 & 0.0220 & 1.86 & 1.08-3.18 & 0.0242 \\ \mbox{Scrap-metal worker} & 197 & 0.07 & 0.05-0.10 & < 0.0001 & 0.08 & 0.05-0.11 & < 0.0001 \\ \mbox{Sinter} & 146 & 1.51 & 1.03-2.20 & 0.0336 & 1.48 & 1.01-2.17 & 0.0436 \\ \hline \mbox{Other exposure circumstances} & & & & & & & & & & & & & & & & & & &$	Grinder	1291	1.82	1.48-2.23	< 0.0001	1.75	1.42-2.15	< 0.0001
Polisher/ molder285 0.81 $0.50-1.32$ 0.4047 0.77 $0.47-1.25$ 0.2826 Solderer80 0.05 $0.03-0.11$ < 0.0001 0.06 $0.03-0.11$ < 0.0001 Surface coater112 0.18 $0.11-0.29$ < 0.0001 0.19 $0.12-0.31$ < 0.0001 Forging-press operator68 1.86 $1.09-3.18$ 0.0220 1.86 $1.08-3.18$ 0.0242 Scrap-metal worker197 0.07 $0.05-0.10$ < 0.0001 0.08 $0.05-0.11$ < 0.0001 Sinter146 1.51 $1.03-2.20$ 0.0336 1.48 $1.01-2.17$ 0.0436 Other exposure circumstancesChemical workers183 0.51 $0.35-0.73$ 0.0003 0.56 $0.38-0.81$ 0.0020 Manufacture of accumulators50 1.58 $0.88-2.85$ 0.1273 1.69 $0.93-3.06$ 0.0823 Manufacture of batteries219 2.01 $1.47-2.76$ < 0.0001 2.05 $1.49-2.82$ < 0.0001 Manufacture of glass178 1.13 $0.88-1.45$ 0.3528 1.17 $0.91-1.51$ 0.2259 Other occupations 337 0.51 $0.42-0.60$ < 0.0001 0.50 $0.40-0.62$ < 0.0001	Chip-remove processor	133	0.28	0.18-0.42	< 0.0001	0.28	0.19-0.43	< 0.0001
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Polisher/ molder	285	0.81	0.50-1.32	0.4047	0.77	0.47-1.25	0.2826
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Solderer	80	0.05	0.03-0.11	< 0.0001	0.06	0.03-0.11	< 0.0001
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Surface coater	112	0.18	0.11-0.29	< 0.0001	0.19	0.12-0.31	< 0.0001
Scrap-metal worker1970.070.05–0.10< 0.00010.080.05–0.11< 0.0001Sinter1461.511.03–2.200.03361.481.01–2.170.0436Other exposure circumstancesChemical workers1830.510.35–0.730.00030.560.38–0.810.0020Manufacture of accumulators501.580.88–2.850.12731.690.93–3.060.0823Manufacture of batteries2192.011.47–2.76< 0.0001	Forging-press operator	68	1.86	1.09-3.18	0.0220	1.86	1.08-3.18	0.0242
Sinter1461.51 $1.03-2.20$ 0.0336 1.48 $1.01-2.17$ 0.0436 Other exposure circumstancesChemical workers183 0.51 $0.35-0.73$ 0.0003 0.56 $0.38-0.81$ 0.0020 Manufacture of accumulators50 1.58 $0.88-2.85$ 0.1273 1.69 $0.93-3.06$ 0.0823 Manufacture of batteries219 2.01 $1.47-2.76$ < 0.0001 2.05 $1.49-2.82$ < 0.0001 Manufacture of glass178 1.13 $0.88-1.45$ 0.3528 1.17 $0.91-1.51$ 0.2259 Other occupations 337 0.51 $0.42-0.60$ < 0.0001 0.50 $0.40-0.62$ < 0.0001 Year of measurement (Ref = 1999) 8052 1.01 $0.99-1.02$ 0.3638 0.99 $0.98-1.01$ 0.4111 Sampling time (log(h)) 8052 0.52 $0.45-0.59$ < 0.0001 $0.99-1.01$ 0.4111	Scrap-metal worker	197	0.07	0.05-0.10	< 0.0001	0.08	0.05-0.11	< 0.0001
Other exposure circumstances Chemical workers 183 0.51 0.35–0.73 0.0003 0.56 0.38–0.81 0.0020 Manufacture of accumulators 50 1.58 0.88–2.85 0.1273 1.69 0.93–3.06 0.0823 Manufacture of batteries 219 2.01 1.47–2.76 < 0.0001	Sinter	146	1.51	1.03-2.20	0.0336	1.48	1.01-2.17	0.0436
Chemical workers 183 0.51 0.35-0.73 0.0003 0.56 0.38-0.81 0.0020 Manufacture of accumulators 50 1.58 0.88-2.85 0.1273 1.69 0.93-3.06 0.0823 Manufacture of batteries 219 2.01 1.47-2.76 < 0.0001	Other exposure circumstances							
Manufacture of accumulators 50 1.58 0.88–2.85 0.1273 1.69 0.93–3.06 0.0823 Manufacture of batteries 219 2.01 1.47–2.76 <0.0001	Chemical workers	183	0.51	0.35-0.73	0.0003	0.56	0.38-0.81	0.0020
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Manufacture of accumulators	50	1.58	0.88-2.85	0.1273	1.69	0.93-3.06	0.0823
Manufacture of glass1781.130.88–1.450.35281.170.91–1.510.2259Other occupations3370.510.42–0.60< 0.0001	Manufacture of batteries	219	2.01	1.47-2.76	< 0.0001	2.05	1.49-2.82	< 0.0001
Other occupations 337 0.51 0.42–0.60 < 0.001 0.50 0.40–0.62 < 0.0001 Year of measurement (Ref = 1999) 8052 1.01 0.99–1.02 0.3638 0.99 0.98–1.01 0.4111 Sampling time (log(h)) 8052 0.52 0.45–0.59 < 0.0001	Manufacture of glass	178	1.13	0.88-1.45	0.3528	1.17	0.91-1.51	0.2259
Year of measurement (Ref = 1999) 8052 1.01 0.99–1.02 0.3638 0.99 0.98–1.01 0.4111 Sampling time (log(h)) 8052 0.52 0.45–0.59 < 0.0001	Other occupations	337	0.51	0.42-0.60	< 0.0001	0.50	0.40-0.62	< 0.0001
Sampling time (log(h)) 8052 0.52 0.45-0.59 < 0.0001	Year of measurement (Ref = 1999)	8052	1.01	0.99–1.02	0.3638	0.99	0.98-1.01	0.4111
	Sampling time (log(h))	8052	0.52	0.45-0.59	< 0.0001			

Abbreviation: CI, confidence interval; FCAW, flux-cored arc welding; GMAW, gas metal arc welding; MEGA, Messdaten zur Exposition gegenüber Gefahrstoffen am Arbeitsplatz; SMAW, shielded metal arc welding; TIG, tungsten inert gas welding.

shielded metal arc welding with coated stick electrodes (SMAW). Median concentrations of $30 \ \mu g/m^3$ or higher were determined in metal sprayers, sinters, forging-press operators and battery-manufacturing workers. The majority of measurements in resistance welders, solderers or brazers, surface coaters such as flame sprayers and scrap-metal workers were below LOQ.

Table 3 depicts the adjusted effect estimates from the regression model as factors modifying the exposure level based on the measured and imputed Ni concentrations. GMAW served as reference group and had higher Ni concentrations than other welding processes such as flux-cored arc welding (FCAW), TIG, laser, submerged arc and resistance welding. The Ni content of the welding material (mainly of the consumable) was associated with a 10-fold difference of the airborne Ni concentration between low (< 5%) and high content (> 30%). Metal sprayers and workers in the production of batteries had at least

twofold higher concentrations than GMAW welders. No time trend in the Ni concentrations could be observed in the data investigated. The concentrations decreased with increasing sampling time.

Table 4 shows the model-based GMs for different occupational tasks estimated for the year 1999 with and without adjustment for the average sampling duration of 2 h. The Ni exposure levels varied widly by major welding process and Ni content of welding materials according to the pattern already found in the raw data: When adjusting for 2 h sampling time, high GMs were estimated for welding materials of high Ni content with GMAW (48 μ g/m³; 95% CI 32–72 μ g/m³) and SMAW (37 μ g/m³; 95% CI 24–57 μ g/m³), respectively. When estimating GMs for welders only, the corresponding mean concentrations were non-significantly higher for welding with consumables of high Ni content (GMAW: 68 μ g/m³, 95% CI 47–101 μ g/m³; SMAW: 45 μ g/m³, 95% CI 30–68 μ g/m³)

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 With adjustment for sampling time (MEGA database, 1990–2009)
 With adjustment for 2 h sampling time
 Without adjustment for 2 h sampling time

 Occupations
 Ni content of welding material (%)
 N
 GM (µg/m³)
 95% Cl (µg/m³)
 GM (µg/m³)
 95% Cl (µg/m³)

Welder						
GMAW		1159	13	12-15	15	13–18
	< 5	156	5	4–7	6	4–8
	5-30	405	24	21-29	26	22-31
	> 30	56	48	32-72	61	40-92
FCAW		93	7	4-11	7	4-11
	< 5	11	3	2-5	3	2–5
	5-30	16	12	8-20	13	8-22
	> 30	0	_	_	_	_
TIG	2 50	799	з	2-3	3	3-4
	< 5	18	1	1_2	1	1_2
	5-30	430	5	4-6	6	5-7
	> 30	21	10	7–16	14	9_21
SMΔ\M/	2 30	470	10	8_13	17	10_15
SMAW	< 5	34	4	3_6	5	3_7
	5 30	1/0	10	15_24	22	17.28
	> 30	140	27	73-24	51	22 70
Autogonous wolding	> 30	22	57	24-37	7	2 20
		20	0	2-10	2	5-20
Laser weiding		35	2	1-4	2	1-5
Submerged arc weiding		20	2	1-0	3	1-/
Plasma weiding		64	9	5-16	1	7-20
Resistance weiding		12	1	0-4	1	0-5
Others or not specified		368	14	12-17	17	14-21
Metal worker						
Cutter		259	14	10–19	18	13–25
Metal sprayer		234	33	23-48	43	30–61
Electroplater		875	3	2–3	3	2–3
Foundry worker		350	7	6–9	7	6–9
Grinder		1291	24	21-29	27	23-31
Chip-remove processor		133	4	2–6	4	3–7
Polisher/ molder		285	11	7–17	12	7–19
Solderer		80	1	0-1	1	0-2
Surface coater		112	2	2-4	3	2-5
Forging-press operator		68	25	15-42	29	17-48
Scrap-metal worker		197	1	1–1	1	1–2
Sinter		146	20	14–29	23	16-33
Other exposure circumstances						
Chemical workers		183	7	5-10	9	6–12
Manufacture of accumulators		50	23	13-41	26	15-46
Manufacture of batteries		219	23	20-36	31	24-42
Manufacture of glass		178	15	12-19	18	14-22
Other occupations		337	7	6-8	8	7_9
		557	,	0.0	0	, ,
Abbreviation: CI, confidence interval; FCAW	, flux-cored arc welding	; GM, geometric me	ean; GMAW, g	as metal arc welding	; MEGA, Messda	aten zur Expositior

Abbreviation: CI, confidence interval; FCAW, flux-cored arc welding; GM, geometric mean; GMAW, gas metal arc welding; MEGA, Messdaten zur Exposition gegenüber Gefahrstoffen am Arbeitsplatz; SMAW, shielded metal arc welding; TIG, tungsten inert gas welding.

(data not shown). Furthermore, high GMs were estimated in metal sprayers (33 μ g/m³), in the manufacture of batteries (27 μ g/m³) and in forging-press operators (25 μ g/m³). The estimates of GMs were higher for most occupations when not adjusting for sampling time, but usually lower than the median concentrations. The variability of Ni concentrations between different occupational settings was high (98.1%), whereas the differences within the same setting were low (1.9%).

DISCUSSION

Using a comprehensive data set of 8052 concentrations of inhalable Ni collected in workers' breathing zone, we estimated the average exposure level in occupations with recognized Ni exposure. Ni occurs mostly as oxides in welding fumes, but also in

a variety of compounds at other workplaces, for example, in Ni refining.⁴ The concentrations were compiled as total Ni in the German exposure database MEGA,¹⁶ together with supplemental information on sampling duration, analytical method, job task and related data. Notably, no data were available for Ni refining. The Ni concentrations were log-normally distributed, where the average should be presented by GM (13.7 μ g/m³) or median (9 μ g/m³) as a robust measure.

The arithmetic mean $(132 \,\mu\text{g/m}^3)$ is much higher due to few high concentrations. The 95th percentile was 460 $\mu\text{g/m}^3$ and 27% of all measurements were below LOQ. Nearly every other concentration of inhalable Ni was above the proposed OEL of 10 $\mu\text{g/m}^3$ of SCOEL.⁵ The 95th percentiles for performing GMAW or SMAW with materials of high Ni content, grinders, cutters and sinters were higher than the current US PEL of 1000 $\mu\text{g/m}^3$. There

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is a large difference between recommended and permitted exposure limits. OELs can additionally vary by the form of Ni (elemental, soluble and insoluble compounds) and particle-size fraction (inhalable, respirable or total dust).²⁴ Exposure limits recommended by scientific committees are usually low, based on scientific evidence of health effects. Permitted limits can be adopted to follow these recommendations. The technical feasibility can be challenging. Welding techniques such as GMAW can hardly comply with 10 μ g/m³ as recommended by SCOEL.

We could not observe a time trend for the measurements between 1990 and 2009 in our data, whereas a decrease of 1.2% per year was found in a larger data set containing concentrations from 1977 to 2009.²⁵ As our data set was part of this analysis for the SYNERGY project (synergy.iarc.fr), we focus on the discussion of the exposure to Ni in welders, where we could use additional information from the MEGA database.

Our analysis can contribute to guantitative estimates of occupational exposure to airborne Ni in JEMs, especially for welders. In 1993, Gerin et al.¹² published a welding process exposure matrix for a cohort study of European welders, in which the job axis was stratified by major technique and type of steel welded. Whereas a limited number of measurements was available to derive the quantitative exposure levels of this JEM,13 more than 3000 personal measurements for welders were compiled in this study based on MEGA. The welding process and Ni content of the material were major determinants of the average exposure concentration ranging between 1 and 50 µg/m³ for the usual 2 h sampling duration. Welding with consumables of high Ni content (>30%) was associated with 10-fold higher concentrations compared with welding with consumables of low content (<5%). Our adjusted GMs of SMAW $(37 \mu g/m^3)$ and TIG $(10 \,\mu\text{g/m}^3)$ for welding materials of high Ni content were similar to the shift concentrations incorporated in the JEM of Gerin et al.¹ (30 and 10 µg/m³, respectively). The highest GM in welders was observed for GMAW (48 μ g/m³) when working with consumables of high Ni content. Even higher average concentrations up to about 100 µg/m³ can occur when welding with high-emission techniques such as GMAW or FCAW is performed in confined spaces. 26,27 The 8 h shift average of 150 $\mu g/m^3$ for GMAW applied to stainless steel in the JEM of Gerin et al.¹² is likely an overestimation. The application of a welding process JEM to populationbased studies requires supplemental questionnaires to capture more detailed technical information on the welding process.²⁸ The job title "welder" is not sufficient to capture the wide range of Ni exposure occurring with different welding techniques. This, for example, is of major importance when investigating the doseresponse relation between Ni in combination with Cr(VI) and lung cancer in welders.

The modelling of average exposure concentrations is pivotal in the development of quantitative JEMs. The strength of our model is the large number of airborne Ni concentrations and detailed information on job tasks and sampling. A challenge in using concentrations from exposure databases, also for monitoring exposure with regard to OELs, is the calculation of an 8 h shift exposure. In practice, welding is usually performed for less than 8 h. Measurements compiled in MEGA lasted on average 2 h and were preferentially conducted during the actual welding process. As a consequence, the GMs predicted from 2 h measurements are rather partial-workshift samples than full-shift time-weighted averages. As the duration of measurements is not independent from the exposure level, we estimated GMs with and without adjustment for sampling duration. As the duration of 62% measurements was 2 h, both GMs were mostly similar. The adjustment to a fixed sampling time of 2 h was based on the functional relation between sampling time and Ni concentration. However, this function can underestimate the concentration in certain exposure circumstances with a high airborne concentration, where the filters are loaded within a shorter time. On the other hand, such a function may overestimate the concentration, for example, in few welders, as the arc time can be shorter than the duration of sampling. We further refrained from the implementation of the analytical methods into the model, as they can depend on the concentration. A more sensitive method was applied following concentrations < LOQ in the analysis of the respective sample with a standard method.

A major challenge is the estimation of mean exposure levels with regard to representativeness.^{20,29} Measurements are usually not conducted as random samples of workplaces. Welding is more frequently applied to join parts of mild steel than of stainless steel.³⁰ However, welders of mild steel and job tasks with low exposure are less frequently monitored than workers with an anticipated high level of exposure. This can bias the estimate of the average exposure level towards higher concentrations, for example if the job title is simply "welder" and no other information available. This underlines the need for supplemental questionnaires when estimating occupational cancer risks, especially in community-based studies.

CONCLUSIONS

This statistical analysis of inhalable Ni concentrations compiled in the German MEGA database aimed at providing exposure estimates for occupations with anticipated exposure. The exposure levels varied strongly between jobs. In welders, exposure was strongly influenced by the major technique and the Ni content of the processed material. High exposures could be also found in grinders, cutters, sinters and metal sprayers. These exposure profiles are useful for exposure assessment in epidemiologic studies and in industrial hygiene. In order to assess exposure to Ni and other occupational carcinogens in community-based studies, supplemental information on job tasks, workplaces and processed materials is essential in addition to job titles.

CONFLICT OF INTEREST

The authors declare no conflict of interest.

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